

Errata to SPIE Vol. TT32 (First Printing):

Design and Mounting of Prisms and Small Mirrors in Optical Instruments

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p. 128 Eqs. (7.2) through (7.4) should read:

$$\Delta = (K_A - K_B)P/t^3,$$

$$\text{where } K_A = \frac{3(m^2 - 1)[a^4 - b^4 - 4a^2b^2 \ln(a/b)]}{4\pi m^2 E_M a^2},$$

$$K_B = \frac{[3(m^2 - 1)(m + 1)][2 \ln(a/b) + (b^2/a^2) - 1][b^4 + 2a^2b^2 \ln(a/b) - a^2b^2]}{(4\pi E_M m^2)(b^2)(m + 1) + (a^2)(m - 1)},$$

pp 128–129 **Numerical Example No. 28** should read:

Consider a 15.75-in. (400.05-mm) diameter mirror for a telescope that is to be held in place with a total preload P of 380 lb (1690.3 N) distributed uniformly around the edge of the mirror by a 6061 aluminum flange with ID of 15.500 in. (393.7 mm) and OD of 15.750 in. (400.050 mm). The pertinent parameters are as follows:

$$a = (15.750/2) = 7.875 \text{ in. (200.025 mm)}$$

$$b = 15.50/2 = 7.750 \text{ in. (196.850 mm)}$$

$$\text{Assume: } t = 0.008 \text{ in. (0.203 mm)}$$

$$E_M = 9.9 \times 10^6 \text{ lb/in.}^2 \text{ (} 6.82 \times 10^{10} \text{ N/m}^2\text{)}$$

$$m = 1/0.332 = 3.012$$

From Eqs. (7.2), (7.3), and (7.1):

$$K_A = \frac{3(3.012^2 - 1)[7.875^4 - 7.750^4 - (4)(7.875^2)(7.750^2) \ln(7.875/7.750)]}{(4\pi)(9.9 \times 10^6)(3.012^2)[(7.750^2)(4.102) + (7.875^2)(2.012)]}$$

$$= 1.408 \times 10^{-11}$$

$$K_B = \frac{[3(3.012^2 - 1)(3.012 + 1)][2 \ln(7.875/7.750) + (7.875^2/7.750^2) - 1][7.750^4 + (2)(7.875^2)7.750^2 \ln(7.875/7.750) - (7.875^2)(7.750^2)]}{[(4\pi)(9.9 \times 10^6)(3.012^2)][(3.012 + 1) + (7.875^2)(3.012 - 1)]},$$

$$= 2.250 \times 10^{-13}$$

$$\Delta = (1.408 \times 10^{-11} - 2.250 \times 10^{-13})(380/0.008^3) = 0.0103 \text{ in. (0.262 mm)}$$

This displacement is large enough to be measured with reasonable accuracy so the preload can be expected to be close to the desired value.