

**Page 9**

Minimum Thickness table:

$$t_f^{ss} = 0.55\Phi\sqrt{P\cdot SF/\sigma_f}$$

$$t_f = 0.433\Phi\sqrt{P\cdot SF/\sigma_f}$$

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$$s = \frac{C_{bfs} r^2}{1 + \sqrt{1 - C_{bfs}^2 r^2}} + \frac{u^2 (1 - u^2)}{\sqrt{1 - C_{bfs}^2 r^2}} \sum_{m=0}^M a_m Q_m(u^2)$$

where  $u = \frac{r}{r_{\max}}$

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According to Karow,  $N \approx 6R^2 (1 - \cos \alpha) / \phi_{eff}^2$ .

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When using a **spherometer** with ball feet:

$$s = \left( \frac{y^2}{(R - B)} \right) / \left[ 1 + \sqrt{1 - \frac{y^2}{(R - B)^2}} \right]$$

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Following are the **scale factors** between various errors and their resulting OPDs *after a round-trip path, as in a Fizeau*.

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**Sag reported on ball-circle spherometer:**

$$s = \left( \frac{y^2}{(R - B)} \right) / \left[ 1 + \sqrt{1 - \frac{y^2}{(R - B)^2}} \right]$$

**Approximate spherical block capacity, edge angle  $\alpha$ :**

$$N \approx 6R^2 (1 - \cos \alpha) / \phi_{eff}^2$$

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**Qbfs equation:**

$$s = \frac{C_{bfs} r^2}{1 + \sqrt{1 - C_{bfs}^2 r^2}} + \frac{u^2 (1 - u^2)}{\sqrt{1 - C_{bfs}^2 r^2}} \sum_{m=0}^M a_m Q_m(u^2)$$

$$\text{where } u = \frac{r}{r_{\max}}$$

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**Bend under uniform pressure for plane parallel circular plates, simply supported and clamped:**

$$s_{ss} = \frac{3Py^4(1-\nu)(5+\nu)}{16Et^3}$$

$$s_c = \frac{3Py^4(1-\nu^2)}{16Et^3}$$

**Bend under self-weight for plane parallel circular plate, simply supported at its edge:**

$$s_{ss} = \frac{3py^4(1-\nu)(5+\nu)}{16Et^2}$$

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This entire entry:

**Reflected wavefront per pass, oblique incidence, embedded in index  $n_1$ :**

$$OPD = 4n_1 h \cos(\alpha)$$

should be corrected to:

**Single-pass reflected wavefront, oblique incidence, embedded in index  $n_1$ :**

$$OPD = 2n_1 h \cos(\alpha)$$

**Single-pass transmitted wavefront, oblique incidence, in air:**

$$OPD = h \left[ \sqrt{(n^2 - \sin^2 \alpha)} - \cos \alpha \right]$$